Optimizing Lateral Boundary Conditions at Staircase-shaped Coastlines: Variational Approach.

Christine & Eugene Kazantsev

Unversity Grenoble Alpes & INRIA FRANCE

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Development



Christine & Eugene Kazantsev

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- Finite elements? Expensive...
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- Better interpolation in frames of FD? May be instable...
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- Finite elements? Expensive...
- Better interpolation in frames of FD? May be instable...
- Variational methods ? We can try...

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Particular discretisation for derivatives near the boundary

Boundary conditions are introduced into the model by a particular discretization of operators near the boundary.

To avoid instabilities, we control both BC and their approximation.



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Particular discretisation for derivatives near the boundary

Boundary conditions are introduced into the model by a particular discretization of operators near the boundary.

To avoid instabilities, we control both BC and their approximation.



Derivatives are allowed to change their properties near the boundaries in order to find the best fit with requirements of the model and data.

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Nucleus for European Modelling of the Ocean (NEMO): Rectangular Box Configuration

 $30^{\circ} \times 20^{\circ}$ rectangle with $\frac{1}{4}^{\circ}$ resolution and 5 z levels. $120 \times 80 \times 5$ nodes in (x, y, z) coordinates, 64 time steps per day.

$$\begin{array}{lll} \displaystyle \frac{\partial u}{\partial t} & = & v(\omega+f) - \frac{\partial (u^2+v^2)/2}{\partial x} - w \frac{\partial u}{\partial z} - \frac{\partial A_u^h \xi}{\partial x} + \frac{\partial A_u^h \omega}{\partial y} + \\ & + & \frac{\partial}{\partial z} A_u^z \frac{\partial u}{\partial z} + g \int_0^z \frac{\partial \rho(x,y,\zeta)}{\partial x} d\zeta + g \frac{\partial(\eta+T_c\phi)}{\partial x} \\ \xi & = & \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}, \quad \omega = \frac{\partial u}{\partial y} - \frac{\partial v}{\partial x} \text{ Divergence, Vorticity} \\ w & = & \int_H^z \xi(x,y,\zeta) d\zeta; \ w(x,y,H) = 0 \quad \text{Vertical velocity} \\ A^z & = & 1.2 \times 10^{-4} \frac{m^2}{s}; \ A^h = 200 \frac{m^2}{s}, \quad f = \frac{4\pi}{86400} \sin(lat) \\ \frac{\partial u}{\partial z}\Big|_{w_0} & = & \frac{-0.1 \frac{N}{m^2} \cos\left(B\pi * \frac{lat - 24^\circ}{44^\circ - 24^\circ}\right)}{hz_1\rho_0} \\ \end{array} \right.$$

 $(u_{\perp},\omega)_{\rm Lateral \ Boundary}=0$ (Impermeability and Free-Slip conditions)

Single Gyre Forcing, Impermeability and Free-Slip conditions

Aligned grid and rotated grid



SSH on the aligned grid





SSH on the 45° rotated grid.



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 $(u_{\perp},\omega)_{\rm Lateral \ Boundary}=0$ (Impermeability and Free-Slip conditions)

$$\begin{aligned} \frac{\partial v}{\partial x}\Big|_{\omega_{b}} &= \frac{\alpha_{1}v_{1/2} + \alpha_{2}v_{3/2}}{h} \\ \frac{\partial u}{\partial y}\Big|_{\omega_{b}} &= \frac{\alpha_{1}u_{1/2} + \alpha_{2}u_{3/2}}{h} \\ \frac{\partial v}{\partial y}\Big|_{\omega_{b}} &= \frac{\alpha_{1}u_{-1/2} + \alpha_{2}v_{1/2}}{h} \\ \frac{\partial u}{\partial y}\Big|_{\omega_{b}} &= \frac{\alpha_{1}u_{-1/2} + \alpha_{2}u_{1/2}}{h} \\ \frac{\partial \omega}{\partial x}\Big|_{v} &= \frac{\alpha_{1}\omega_{0} + \alpha_{2}\omega_{1}}{h} \\ \frac{\partial \omega}{\partial y}\Big|_{u} &= \frac{\alpha_{1}\omega_{0} + \alpha_{2}\omega_{1}}{h} \\ \frac{\partial \omega}{\partial y}\Big|_{u} &= \frac{\alpha_{1}\omega_{0} + \alpha_{2}\omega_{1}}{h} \\ \alpha_{1} &= \alpha_{2} = 0 \\ \alpha_{1} &= -1, \quad \alpha_{2} = 1 \\ \alpha_{1} &= -1, \quad \alpha_{2} = 1 \\ \alpha_{1} &= -1, \quad \alpha_{2} = 1 \end{aligned}$$



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The model: $x(t) = \mathcal{M}_{0,t}(x(0), \alpha)$ with $x = (u, v, T, S, ssh)^T$

Cost function ${\cal J}$

$$J = 10^{-4} (\|x(0) - x_{bgr}\|^2 + \|\alpha - \alpha_{bgr}\|^2) + \int_{t=0}^{T} t \int \int (u - u_{ref})^2 + (v - v_{ref})^2 + (ssh - ssh_{ref})^2 dxdydt$$

Layout:

- Joint control of the initial point x(0) (interpolation errors) and the set of α ;
- Artificially generated data by the same model on the aligned grid;
- Data Assimilation over the 50 days window;
- Analysis of the solution on the 8 years interval.
- Minimization is performed by M1QN3 (JC Gilbert, C.Lemarechal);
- Adjoint is generated by Tapenade (Ecuador team, INRIA).

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Single Gyre Control: 45° rotation, SSH

Reference, Optimal and Conventional BC 800 days later





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Single gyre, α_1, α_2



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$$\begin{aligned} \frac{\partial v}{\partial x}\Big|_{\omega_{b}} &= \frac{\alpha_{1}v_{-1/2} + \alpha_{2}v_{1/2}}{h} \\ \frac{\partial u}{\partial y}\Big|_{\omega_{b}} &= \frac{\alpha_{1}u_{-1/2} + \alpha_{2}u_{1/2}}{h} \\ \frac{\partial v}{\partial x}\Big|_{\omega_{b}} &= \frac{\alpha_{1}u_{-1/2} + \alpha_{2}v_{3/2}}{h} \\ \frac{\partial v}{\partial y}\Big|_{\omega_{b}} &= \frac{\alpha_{1}u_{1/2} + \alpha_{2}v_{3/2}}{h} \\ \frac{\partial \omega}{\partial y}\Big|_{u} &= \frac{\alpha_{1}u_{0} + \alpha_{2}\omega_{1}}{h} \\ \frac{\partial \omega}{\partial y}\Big|_{u} &= \frac{\alpha_{1}\omega_{0} + \alpha_{2}\omega_{1}}{h} \\ \frac{\partial \omega}{\partial y}\Big|_{u} &= \frac{\alpha_{1}\omega_{0} + \alpha_{2}\omega_{1}}{h} \\ \alpha_{1} &= 0, \quad \alpha_{2} = -0.1 \\ \alpha_{1} &= -1.4, \quad \alpha_{2} = 0.6 \\ \alpha_{1} &= -1.01, \quad \alpha_{2} = 1.01 \\ \alpha_{1} &= -1.01, \quad \alpha_{2} = 1.01 \end{aligned}$$



$$\omega_{\circ} = rac{\partial v}{\partial x} - rac{\partial u}{\partial y} - 0.8 rac{u+v}{h}$$

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"Optimal" configuration

$$\omega_{o} = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} - \frac{u+v}{h}$$
$$= \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} - \frac{\vec{V}.\vec{\tau}}{h/\sqrt{2}}$$



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$$\begin{split} \omega_{\circ} &= \quad \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} - \frac{u+v}{h} \\ &= \quad \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} - \frac{\vec{V}.\vec{\tau}}{h/\sqrt{2}} \end{split}$$

- Free-slip condition on a curvilinear boundary $\omega|_{bnd} = \frac{\vec{V}.\vec{\tau}}{R}$
- Optimal boundary is curvilinear with $R = -h/\sqrt{2}$



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$$\omega_{\circ} = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} - \frac{u+v}{h}$$
$$= \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} - \frac{\vec{V} \cdot \vec{\tau}}{h/\sqrt{2}}$$

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Variable $R_{30^{\circ}} : -h \le R_{30^{\circ}} \le 5h$.



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The Radius depends on the grid resolution h. Does this curvilinear boundary remains optimal on different resolutions?

Single Gyre Control: 45° rotation, $1^{\circ}/2$ resolution

Reference, Optimal and Conventional BC 800 days later







Rotated grid conventional BC SSH



Rotated grid constant $R = -h/\sqrt{2}$ BC SSH

Single Gyre Control: 45° rotation, $1^{\circ}/8$ resolution

Reference, Optimal and Conventional BC 800 days later





Reference SSH





Rotated grid, constant $R = -h/\sqrt{2}$ BC SSH

Layout:

- NEMO, Global ocean model, 2° resolution, 31 layer;
- ECMWF data issued from Jason-1 and Envisat altimetric missions and ENACT/ENSEMBLES data banque;
- Data Assimilation during 10 days interval;
- Analysis of the distance "model-observations" on 1 month interval

Distance "model-observations"



Layout:

- NEMO, Global ocean model, 2° resolution, 31 layer;
- ECMWF data issued from Jason-1 and Envisat altimetric missions and ENACT/ENSEMBLES data banque;
- Data Assimilation during 10 days interval;
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SSH, North Atlantic, January, 31, 2006.



Optimal Initial Conditions.



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Optimal BC at the bottom.

Conclusion

Boundary Conditions influence is important

- Optimal BCs allows to correct errors committed by the discretization
- The model is closer to the reference one with optimal BC
- Data assimilation allows to get an optimal position and form of the boundary

BUT

As well as for any adjoint parameter estimation

- The control may violate the model physics;
- The physical meaning of the optimal boundary is difficult to understand;
- The set of α is not unique;
- The problem of identifiability is not addressed yet;
- The problem of stability is not even posed.

Consequently:

It is not a parameter estimation study, but

- a way to compensate model errors
- showing the most influent parameter.

Thank you

Another result of the Russian-French cooperation





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